



FWC

G.C.E A / L Examination March - 2018

Conducted by Field Work Centre, Thondaimanaru

In collaboration with

Provincial Department of Education Northern Province

Grade:- 13 (2018)

Physics

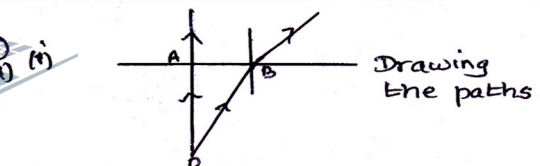
Marking Scheme

	I	II	III	IV	V
1	4	3	2	1	4
2	5	4	4	3	2
3	2	5	3	4	5
4	3	2	3	3	3
5	2	2	2	2	2
6	5	2	1	2	5
7	4	3	5	3	1
8	4	3	2	1	1
9	5	3	2	1	5
10	5	2	1	1	2

Part 1 (M.C.Q)	100
Part II - A (St. Essay)	40
Part II - B (Essay)	60
Total	200
Final	$\frac{200}{2} = 100$

Part II A

- 1 (a) i) $d = \frac{L}{N}$ 1
 ii) 100 1
- (b) i) 0.01 mm 1
 ii) $\frac{0.41 + 0.41 + 0.42 + 0.40 + 0.42}{5}$
 $= 0.412$ mm 1
 d average = 0.41 mm 1
- iii) zero error = -0.03 mm
 \therefore corrected reading = $0.41 + 0.03$
 $= 0.44$ mm 1
- iv) diameter of the spring (x) 1
 Vernier caliper 1
- v) $V = \frac{\pi d^2}{4} \cdot \pi X N$ 2



- (ii) will undergo TIR 1
 (iii) $e n_1 = \frac{n_1}{n_2}$ 1
 (iv) $\frac{n_1}{n_2} = \frac{1}{\sin \theta_c}$; $e n_1 = \frac{1}{\sin \theta_c}$ 1

(b) (i) 1.5

(ii) $\sin \theta = \frac{R-d}{R+d}$ 1

- (iii) will decrease continuously 1
 (iv) No ray will escape when $\theta \geq \theta_c$ 1
 $\sin \theta \geq \sin \theta_c$

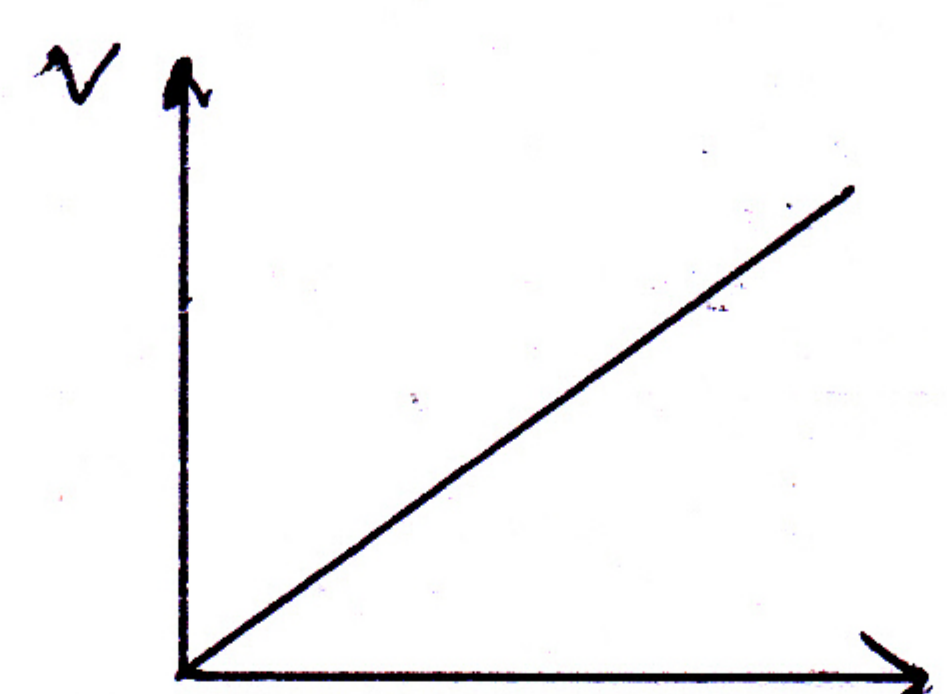
$$\frac{R-d}{R+d} \geq \frac{1.44}{1.5}$$

$$\frac{R-d}{R+d} \geq 0.96 \quad R \geq 490 \text{ mm}$$

$$R_{\min} = 490 \text{ mm} \quad \dots 1$$

- (v) For each application and the corresponding advantage 1+1

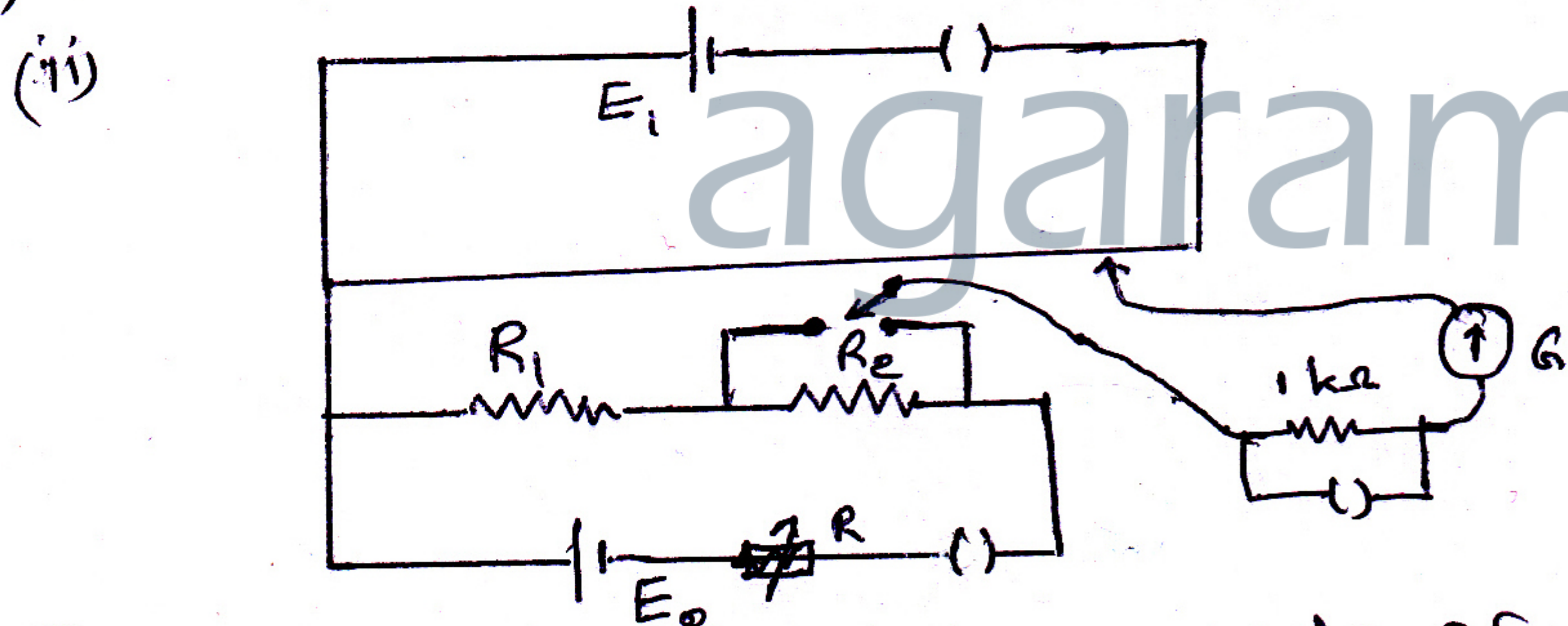
- 3 a) Instrument - Thermometer }
 apparatus - stirrer } 1
- b) Heat the tube (using bunsen burner) and dip the open end in a vessel containing mercury and allow it to cool (for a short period) 1
- c) water vapor will be present if water is used instead. (accept any other suitable answer) 1
- d) In order to ensure the temperature of the dry air is same that of the water bath 1

- e) (i) selection of two points that intersects the grid }
 gradient = $0.1 \text{ cm } ^\circ\text{C}^{-1}$ 1
- (ii) $0.1 = \frac{27}{x} \Rightarrow x = 270^\circ\text{C}$ (To find the intercept) 1
 Absolute zero temperature = -270°C 1
 (Accept $-265 \rightarrow -275^\circ\text{C}$)
- (iii) reason: Volume is assumed to be proportional to the length
 (of air column) 1
 property: uniform internal cross section / diameter 1
- iv)  1
- f) To increase the sensitivity of the tube /
 To obtain a good distribution of experimental points 1

(4) (a) E_1 - should provide constant current,
 PQ - possesses uniform cross sectional area /
 thin wire with uniform diameter / uniform resistive wire 1

- (b) (i) X 1
 (ii) $\frac{V_1}{V_2} = \frac{R_1}{R_1 + R_2}$ 1

(c) (i) in order to protect the galvanometer 1



(iii) by touching the two ends of the potentiometer
 and check whether the deflections of the centre
 zero galvanometer are in the opposite directions 1

d (i) $\frac{R_1}{R_1 + R_2} = \frac{l_1}{l_2}$; $\frac{l_2}{l_1} = 1 + \frac{R_2}{R_1}$ 1

(ii) by changing the resistance of the resistance box; R 1

(iii) gradient of the l_2 vs l_1 graph is $1 + \frac{R_2}{R_1}$

$1 + \frac{R_2}{R_1} = 1.5$

$\frac{R_1}{R_2} = 2$ 1

- ⑤ (a) (i) $\tau = Fr$
 $\tau = I\alpha$ α - angular acceleration
 $\alpha = \frac{Fr}{\frac{1}{2}Mr^2} = \frac{2F}{Mr}$
- (ii) Since the torque is same as before in a(i) $\alpha = \frac{2F}{Mr}$
- (b) (i) $\Sigma \tau = 0$, condition for equilibrium
 If T is the tension in the rope then
 $T \times 0.1 = 200 \times 0.8$
 $T = 1600 \text{ N}$
- (ii) less than that calculated
- (c) (i) New tension in the rope = 3200 N (force doubled)
 weight of the boat = 3200 N
 mass of the boat = 320 kg
- (ii) minimum work done = gain in P.E = $320 \times 10 \times 2$
 = 6400 J
- (d) (i) If the tension in the rope is T' ,
 $400 \times 0.8 = T' \times 0.1 + \tau_{\text{frictional}}$
 $= T' \times 0.1 + 4$
 $T' = 3160 \text{ N}$
 Frictional force acting on the boat = 3160 N
- (ii) angular speed of the cylinder, $\omega = \frac{v}{r} = \frac{0.2}{0.1} = 2 \text{ rad s}^{-1}$
 \therefore Total power loss against friction and frictional torque = $\tau \omega$
 = $400 \times 0.8 \times 2$
 = 640 W
- Can use $F \cdot v + \tau_f \omega$ alternatively
- (iii) angular deceleration $\alpha = \frac{\tau}{I} = \frac{4}{\frac{1}{2} \times 100 \times 0.1^2} = 8 \text{ rad s}^{-2}$
 using $\omega = \omega_0 + \alpha t$
 $0 = 2 - 8 \cdot t$
 $t = 0.25 \text{ s}$
 comes to rest in 0.25 s

- ⑥ (i) Stating any 3 differences between P and S waves { All } 2
 { Any two } ①
- (ii) (a) ; Direction of propagation of wave and the direction of vibration are parallel to each other. 1+1
- (iii) $D_1, D_2, P_3, D_4, D_5, D_6, D_7, D_8$ (or in the reverse order) 1
- (iv) direct pulse - 0.4 s } 1
 reflected pulse - 0.6 s }
- (v) speed = 3 km s⁻¹
 $Mx + x D_8 = 3 \times 0.6 = 1.8 \text{ km}$
 $M D_8 = 3 \times 0.4 = 1.2 \text{ km}$

contd

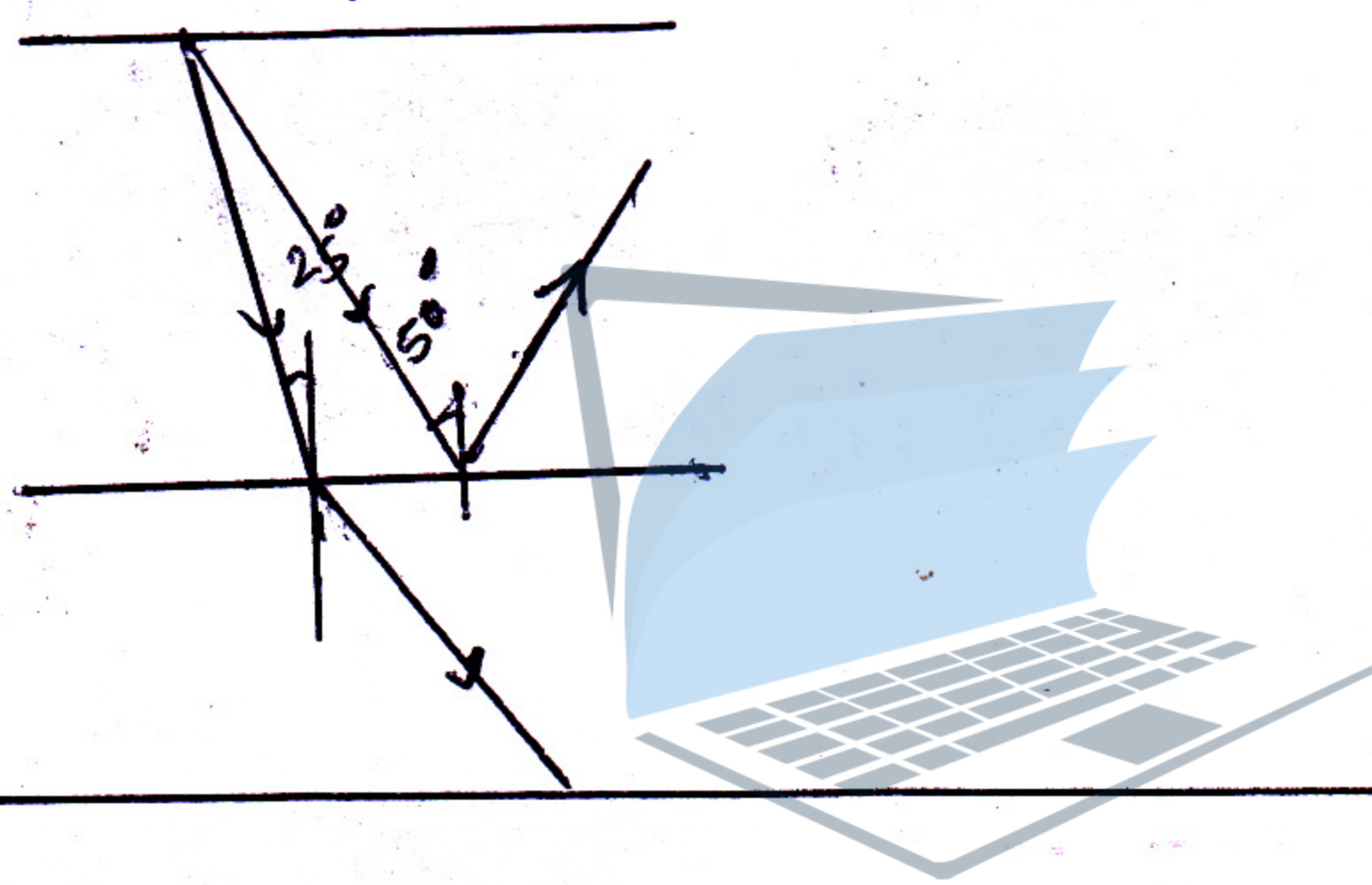
If thickness of the rock is d , $d = \sqrt{Mx^2 - \left(\frac{MD_s}{2}\right)^2}$
 $= \sqrt{0.9^2 - 0.6^2} = 0.3\sqrt{3^2 - 2^2} = 0.3\sqrt{5}$
 $= 0.672 \text{ km} \quad (0.62 - 0.72 \text{ km})$

(vi) $A = v_p^2 \rho$
 $= 3000^2 \times 2700 = 2.43 \times 10^{10} \text{ kg s}^{-2} \text{ m}^{-1} = 2.43 \times 10^{10} \text{ Pa}$
 (Do not award this mark if unit is wrong)

(vii) rock sample may have irregular boundary / the rock boundary not horizontal / sample is not homogeneous } wave encountering intermediate different layer (accept any other possible answers)

(b) (i) refractive index of the second medium (vel. 5 km s^{-1}) w.r. to the rock medium $= \frac{3}{5} = 0.6000$
 critical angle c is given by $\sin c = 0.6$
 $c = 37^\circ$

(ii)



- (7) A - Proportional limit }
 B - Elastic limit }
 C - Breaking point }
 Distinguishing A and B

All correct only 2

(a) (i) Young's modulus of steel, $y_s = \frac{3 \times 10^8}{1.5 \times 10^{-3}} = 2 \times 10^{11} \text{ N m}^{-2}$
 Young's modulus of copper, $y_c = \frac{2 \times 10^8}{2 \times 10^{-3}} = 1 \times 10^{11} \text{ N m}^{-2}$

(ii) For steel wire, max^m load (without exceeding proportional limit)
 $F_1 = 3 \times 10^8 \times 0.8 \times 10^{-6} = 240 \text{ N}$

For copper wire, max^m load (without exceeding proportional limit)
 $F_2 = 2 \times 10^8 \times 0.8 \times 10^{-6} = 160 \text{ N}$

(iii) Maximum load on the composite wire = 160 N

(b) Force on a wire, $F = \frac{A y e}{l}$

Each wire is extended by 1 mm (to identify)

$F = \frac{0.8 \times 10^{-6} \times 2 \times 10^{11} \times 1 \times 10^{-3}}{2} = 80 \text{ N}$

Contd

Weight to be placed at the centre = $4 \times 80 \text{ N} = 320 \text{ N}$.

mass = 32 kg

(e) (i) Let the forces acting on the steel and copper wires are F_s and respectively.

$F \propto AY$ (e + l same for each)

$$\frac{F_s}{F_c} = \frac{0.8 \times 2 \times 10^{11}}{2.4 \times 1 \times 10^{11}} = \frac{2}{3}$$

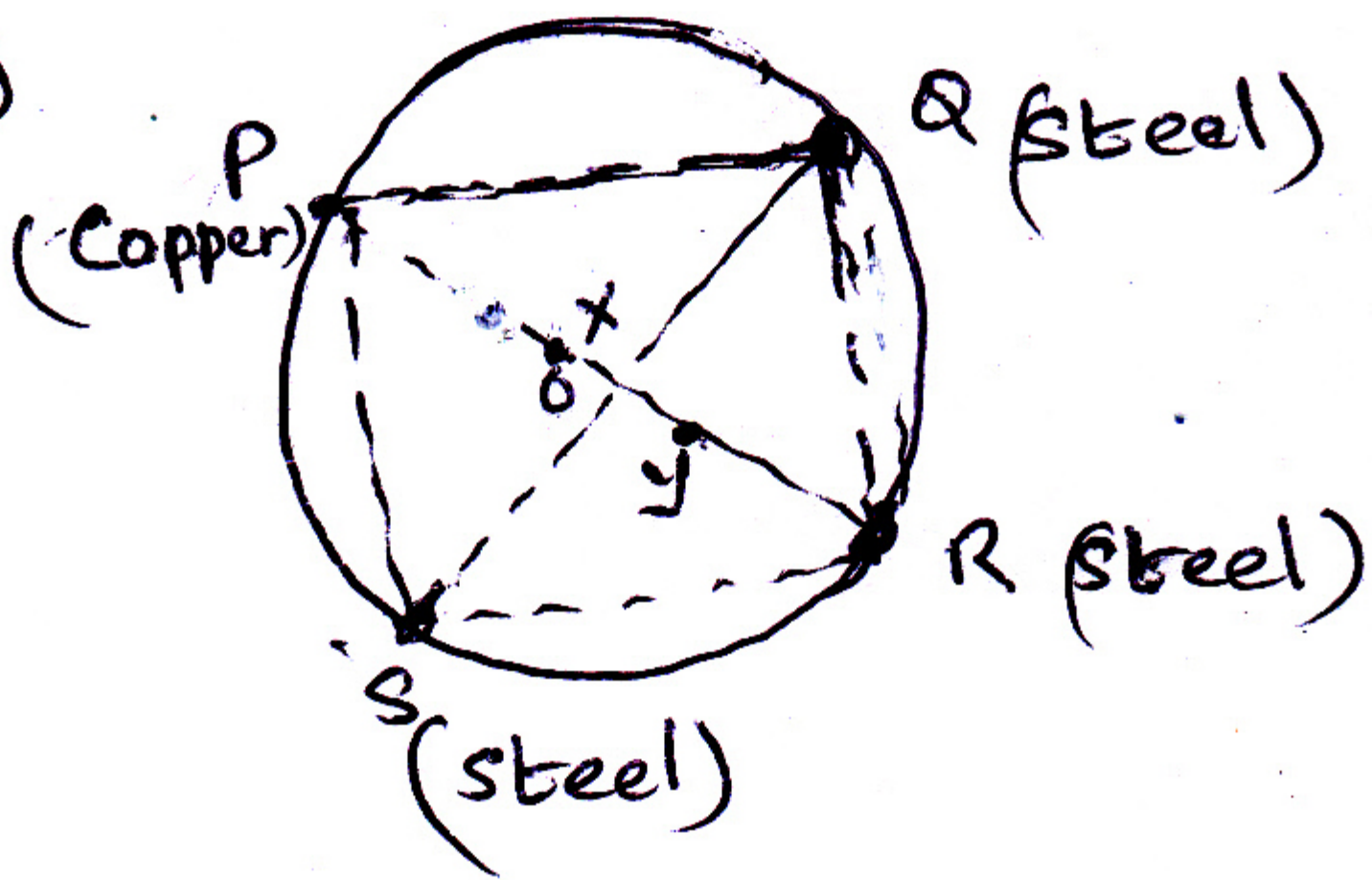
(ii) Force acting on the copper wire $F_c = \frac{2.4 \times 10^{-6} \times 1 \times 10^{11} \times 1 \times 10^{-3}}{2}$

$$= 120 \text{ N}$$

Tension on one of the steel wires = $\frac{2}{3} \times 120 = 80 \text{ N}$

\therefore Total weight = $120 + 3 \times 80 = 360 \text{ N}$

(ii)



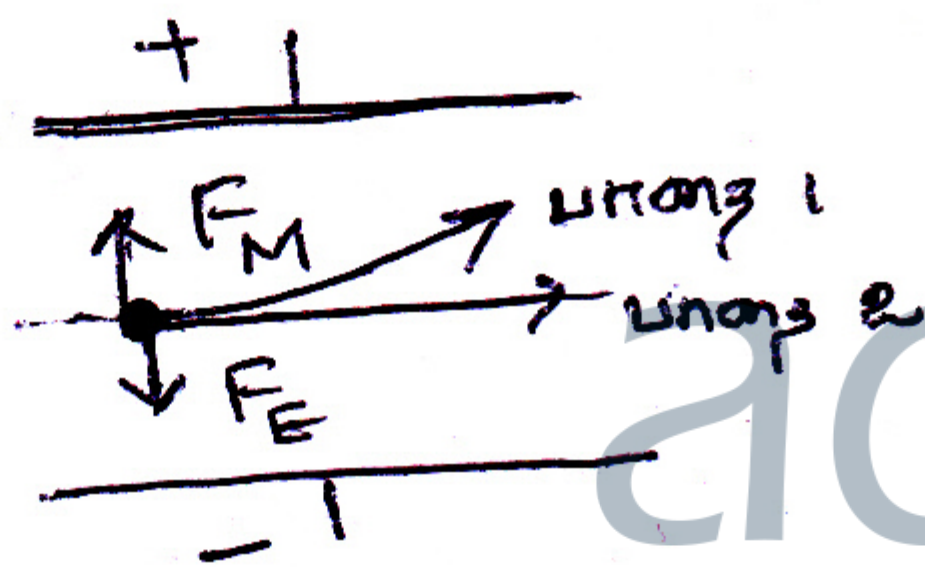
Resultant of the tensions due to 3 steel wires passes through Y, such that $OY = \frac{1}{3} OR = 2.5 \text{ cm}$

Resultant of all four wires acts at X. (Mark X on the diagram)

$$\frac{PX}{XY} = \frac{240}{120} = 2$$

$$PX = \frac{2}{3} \times PY = \frac{2}{3} \times 10 = 6.67 \text{ cm}$$

8 (a) (i)



For denoting F_E and F_M

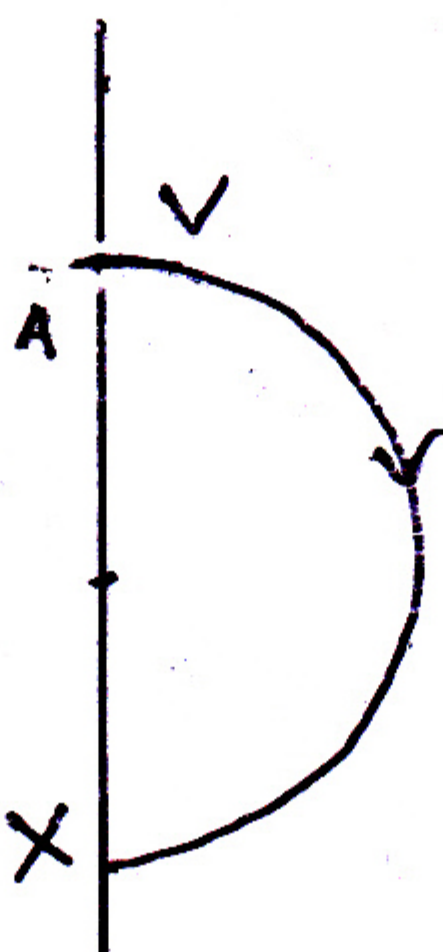
(ii) 1. } For drawing paths 1 and 2

(iii) For undeviated particle, $F_E = F_M$

$$qE = BqV \Rightarrow V = \frac{E}{B}$$

(b) (i) Circle | Part of a circle. Magnetic force is always perpendicular to the path of the particle.

(ii)



(iii) V, No work is done by the magnetic field

(iv) Magnetic force = $B_0 qV$

$$\text{centripetal acceleration} = \frac{V^2}{r}$$

r - radius

$$\text{Using } F=ma, B_0 qV = m \frac{V^2}{r}$$

for LHS and RHS

$$r = \frac{mV}{B_0 q} = \frac{m}{B_0 q} \Rightarrow \alpha = \frac{2mV}{B_0 q} = \frac{2mE}{B_0 qB}$$

(c) (i) M_1 (ii) For isotope with mass M_1 , $AX = \frac{2 M_1 E}{B_0 q B}$

$$M_2, AY = \frac{2 M_2 E}{B_0 q B}$$

Separation $xy = AX - AY$

$$d = \frac{2 (M_1 - M_2) E}{B_0 q B}$$

$$(iii) d = \frac{2 (M_1 - M_2) v}{B_0 q B}$$

$$= \frac{2 \times (6.17 \times 10^{-26} - 5.87 \times 10^{-26}) \times 500}{2 \times 10^{-3} \times 1.6 \times 10^{-19}}$$

$$= 9.375 \times 10^{-3} \text{ m}$$

$$(c) (i) R = \frac{\rho l}{A}$$

 ρ - Resistivity l - length A - cross sectional area

$$(ii) V = Al = \text{constant}$$

$$R = \frac{\rho l}{V/l} = \rho l^2$$

$$\therefore R \propto l^2$$

(b) (i) length of the wire could be increased and hence the change in resistance will be significantly high

$$(ii) 8 \times 0.075 \text{ m} = 0.60 \text{ m}$$

$$(iii) R = \frac{\rho l}{A} = \frac{5 \times 10^{-7} \times 0.6}{\pi \times (0.02 \times 10^{-3})^2} = \frac{75}{\pi} \times 10 = 239 \Omega$$

$$(iv) 239 \propto 0.600^2$$

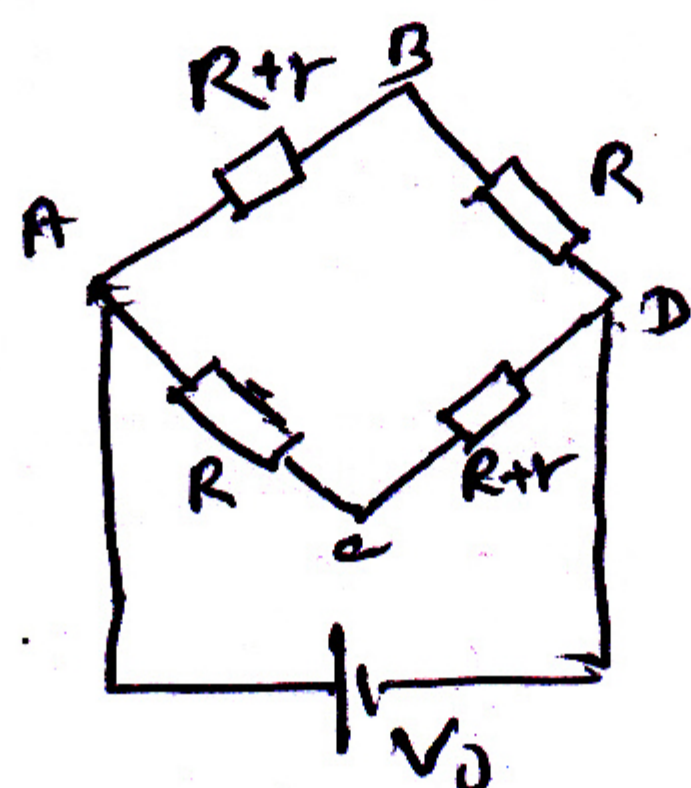
change in resistance $\Delta R \propto 2 \times 0.600 \times 0.001$

$$\frac{\Delta R}{239} = \frac{2 \times 0.001}{0.600} = \frac{1}{300}$$

$$\therefore \Delta R = 0.800 \Omega$$

(c) i. 0 V

ii.



Potential drop across A and B = $\frac{V_0 \cdot (R+r)}{R+r+R}$

Potential drop across A and C = $\frac{V_0 \cdot R}{R+R+r}$

$$\therefore \text{p. drop across B and C} = \frac{V_0 (R+r)}{2R+r} - \frac{V_0 R}{2R+r} = \frac{V_0 r}{2R+r}$$

$$\therefore \text{Voltmeter reading} = \frac{V_0 r}{2R+r}$$

Q9A contd

*Least count of the voltmeter = 0.01 V
 Minimum change in resistance corresponds to 0.01 V

$$\frac{V_0 r_{\min}}{2R + r_{\min}} = 0.01 \quad V_0 = 10 \text{ V}, R = 239 \Omega$$

$$\therefore r_{\min} = 0.48 \Omega$$

(a) (i) I-V characteristics of a Zener diode
 denoting V_z (Zener breakdown voltage)

P.d across the device = 10 V

\therefore p.d across R = 12 - 10 = 2 V

$$\text{Current through R, } I_R = I_{\text{Load}} + I_Z = \frac{10}{100} + \frac{10}{1000} \text{ A} = 0.11 \text{ A}$$

$$R = \frac{2}{0.11} = 18.18 \Omega$$

(ii) If the voltmeter is assumed to function when voltage (supply) increases to 15 V the current through R would be $I_R = \frac{5}{18.18} = \frac{5}{200/11} = 275 \text{ mA}$

The current through the load = 100 mA
 current through zener = 175 mA

This is impossible (max^m current = 65 mA)

(iii) Maximum allowed current through R is

$$(I_R)_{\max} = 100 + 65 \text{ mA} = 165 \text{ mA}$$

$$\text{maximum p.d across R is } (V_R)_{\max} = \frac{165}{1000} \times \frac{200}{11} = 3 \text{ V}$$

\therefore Maximum of the source voltage = 10 + 3 = 13 V

(b) (i) $V_{R_1} = 6 - 0.6 = 5.4 \text{ V}$

(ii) Base current $I_B = \frac{5.4}{R_1} = \frac{5.4}{100 \times 10^3} = 5.4 \times 10^{-5} \text{ A} = 54 \mu\text{A}$

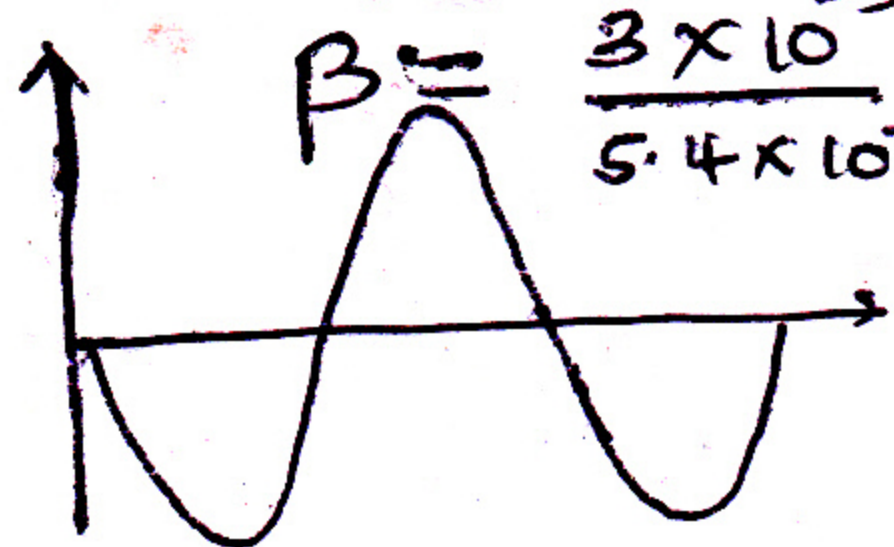
(iii) Current gain $\beta = \frac{I_C}{I_B}$

$$V_{R_2} = 6 - 3 = 3 \text{ V}$$

$$I_C = \frac{3}{R_2} = \frac{3}{1 \times 10^3} \text{ A} = 3 \times 10^{-3} \text{ A} \quad (3 \text{ mA})$$

$$\beta = \frac{3 \times 10^{-3}}{5.4 \times 10^{-5}} = 55.6$$

(iv)



(Note the change in phase + increased amplitude)

$$(10) (i) P = P_0 + \frac{Mg}{A}$$

$$(ii) \text{ Pressure at } 27^\circ\text{C} = 1 \times 10^5 + \frac{12 \times 10}{25 \times 10^{-4}} = 1.48 \times 10^5 \text{ Pa}$$

(iii) Pressure remains constant $\therefore \frac{V}{T} = \text{const}$

$$1. \quad \frac{Ah}{300} = \frac{Ah'}{330} \quad h' - \text{new height at } 57^\circ\text{C}$$

$$2. \quad h = 20 \text{ cm}; \quad h' = 22 \text{ cm}$$

$$\Delta W = P \Delta V$$

$$= 1.48 \times 10^5 \times 2 \times 25 \times 10^{-6}$$

$$= 7.4 \text{ J}$$

$$3. \quad \eta = \frac{PV}{RT} = \frac{1.48 \times 10^5 \times 25 \times 20 \times 10^{-6}}{.25/3 \times 300} = 0.0296 \text{ mol}$$

$$4. \quad \frac{P_{27}}{300} = \frac{P_{57}}{330}$$

$$\frac{1.48 \times 10^5}{300} = \frac{P_{57}}{330}$$

Pressure at 57°C is $1.628 \times 10^5 \text{ Pa}$

If the load that brings the piston to its original position is M' ,

$$\frac{M'g}{A} = 1.628 \times 10^5 - 1 \times 10^5$$

$$= 0.628 \times 10^5 \text{ N m}^{-2}$$

$$M' = \frac{0.628 \times 10^5 \times 25 \times 10^{-4}}{10} = 15.7 \text{ kg}$$

\therefore additional load = $15.7 - 12 = 3.70 \text{ kg}$

$$(b) (i) \text{ Pressure inside the vessel} = 1 \times 10^5 + \frac{25 \times 10}{25 \times 10^{-4}}$$

$$(ii) \text{ Temperature corresponds} = 2 \times 10^5 \text{ Pa}$$

$$\text{to this pressure} = 130^\circ\text{C}$$

(iii) Yes. Since the pressure in the region surrounding water becomes equals to SVP of water.

$$(c) (i) 8000 \text{ Pa.}$$

$$(ii) R.H = \frac{\text{S.V.P at dew point}}{\text{SVP at air temp}} \times 100 \%$$

$$50 = \frac{\text{SVP at dew point} \times 100}{8000}$$

$$\text{S.V.P. at dew point} = 4000 \text{ Pa}$$

$$\text{dew point temp} = 26^\circ\text{C}$$